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(54) Vaporization contact laser probe

Bei Gewebeberührung Verdampfung verwischende Lasersonde

Sonde laser effectuant une vaporisation au contact du tissu

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(56) References cited:
EP-A- 0 038 281
EP-A- 0 157 593
WO-A-84/04879
GB-A- 2 154 761

EP-A- 0 131 341
EP-A- 0 178 464
WO-A-85/05262

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Description

This invention relates to a medical laser probe for effecting incision or vaporisation with respect to tissues of human or animal organisms and to a process for making a medical laser probe. More specifically, the present invention pertains to a dual mode laser surgical probe which achieves tissue vaporisation by the combined heating occasioned by direct laser irradiation of the tissue as well as by heating of the laser tip which, in turn, is brought into contact with the tissue in which the incision is being made.

Laser surgery of a non-contact variety has been known for many years. In general, the simplest form of non-contact laser surgery utilises a flexible quartz fiber for transmitting laser energy from a Nd:YAG laser source to the tissue undergoing treatment. In this system, the end of the quartz fiber serves as the probe for irradiating the tissue to effect incision or coagulation thereof. The fiber tip, however, must be maintained in spaced relationship to the tissue to avoid fouling of the fiber and, importantly, to avoid heat damage to the fiber end. Non-contact laser systems utilising a laser transmissive member at the output end of the fiber to focus or otherwise alter the radiation characteristics of the fiber have also been proposed, for example, by Enderby, US Patent No. 4273109.

Such non-contact laser irradiation systems, however, exhibit poor operating efficiency as well as poor reproducibility. In general, it is necessary to maintain a fixed spacing between the output end of the laser probe or fiber and the tissue undergoing treatment in order that the laser energy density at the tissue remains constant. However, in the conventional non-contact laser irradiation system, it is difficult to keep the distance constant, especially when the surgical procedure is being performed remotely through use of an endoscope. In addition, the non-contact irradiation system exhibits a significant disadvantage in that the laser beam is back-scattered from the surface of the tissue and a considerable percentage of the radiated laser energy is lost.

The inventor of the present invention has previously proposed an improved probe having a tip member which is made, for example, of an artificial sapphire disposed in front of an optical fiber through which the laser energy passes enroute the tissue undergoing treatment. Thus, in WO 85/05262 there is disclosed a medical laser probe for conveying laser energy from the output end of an optical laser waveguide to a tissue undergoing laser treatment the probe comprising a laser transmissive material having a laser energy input region for receiving laser energy from an optical waveguide and a laser energy radiation surface, the laser energy from the input region being propagated through the probe transmissive material to be incident on the probe radiation surface, the probe radiation surface being in the form of a melt which contains bubbles such that the melt is translucent to a degree of 20 to 50%. In view of the properties of the tip member, in par-

ticular, its higher melting temperature, the probe can be maintained in direct contact with the tissue with a corresponding improvement in procedure efficiency and reproducibility.

This new contact laser irradiation system, however, still requires substantial output from a laser generating unit, often in excess of 40 to 50 watts for incision or vaporization, although the required output depends upon the mode of treatment. The necessitates use of a large-scale laser generating unit, including its associated bulky power supply, which is expensive and non-portable. The laser probe of the present invention produces the required tissue heating at substantially reduced laser power levels.

WO-A-84/04879 describes a laser probe which comprises an infrared absorbing element whereby the predetermined percentage of the laser energy which is converted into heat is approximately 100%. The infrared absorbing element is covered with a coating of laser transmissive material, which coating serves to provide for easy release from the tissue and for mechanical protection of the element.

GB-A-2154761 discloses a diffusive optical fibre tip for surgical applications. Diffusion is achieved by covering the fibre tip with a resin compound impregnated with fine particulate powder so as to give a reflective or refractive effect.

According to the present invention there is provided a medical laser probe for conveying energy from the output end of an optical laser waveguide to a tissue undergoing laser treatment, the probe comprising laser transmissive material having a laser energy input region for receiving laser energy from the optical waveguide and a laser energy radiation surface, the laser energy from the input region being propagated through the probe transmissive material to be incident on the probe radiation surface, characterised in that an infrared absorbing coating is applied to and conforming with the laser energy radiation surface for converting a predetermined percentage of the laser energy incident thereon into heat energy, whereby the increased temperature of the probe radiation surface will enhance tissue vaporisation and whereby the laser energy entering the probe not converted to heat energy by the infrared absorbing coating irradiates tissue adjacent the radiation surface.

More specifically a laser probe has its outside radiating surface covered with a thin coating of infrared absorbing material such as manganese dioxide (MnO_2). The manganese dioxide absorbs some of the laser energy as it passes from the probe thereby heating the tip region of the probe to, for example, about 700°C. When the heated outer surface of the probe is brought into contact with the tissue, the tissue adjacent thereto is carbonised due to the heat. Thus, vaporisation of the surface tissue is significantly enhanced. However, as noted, all of the laser energy is not absorbed by the infrared absorbing material and a part of the laser beam is passed directly to the tissue. The direct irradiation of the tissue enhances the vaporisation of the carbonised

tissue as it passes therethrough into the tissue below. Thus, the vaporisation is further accelerated. The passage of the radiated laser beam through the carbonised layer advantageously performs a hemostasis effect in the tissue.

In the conventional probe, there is little vaporisation of the tissue directly due to probe heat, rather, vaporisation is limited by the reaction within the tissue of the laser energy as it penetrates into the tissue. In the present invention, by contrast, vaporisation is not limited to heat generated by direct laser irradiation but includes the heat of the probe tip as it is brought into physical contact with the tissue. This heat, as noted, is generated by reason of the absorption of laser energy in the coated surface of the probe tip.

In this connection, it is to be noted that while an output from the laser generating unit of 40W or more is needed in the conventional probe for vaporization, 5 to 10W, or in some cases, even 1 to 5W will suffice in the probe of the present invention or effecting vaporization or incision.

The infrared absorbing material may be deposited on the smooth surface, but it is preferably deposited in concaved portions of an uneven, roughened outer surface of the probe. In the latter case, the infrared absorbing coating is generally protected against being dislodged or detached and there is the further advantage that irregular laser reflections within the concaved portions of the tip serve to enhance laser interaction with the surface absorbant material thereby accelerating heat generation.

Since the fine particles of heat absorbing material may, notwithstanding the improved adherence of this material to the roughened surface, become dislodged or possibly subjected to oxidation, a protective coating of heat-resistant ceramic material is preferably placed over the heat absorbing tip end of the probe. The coating, of course, must be substantially transparent to the laser energy.

The present invention further provides a method for making a medical laser surgical probe having a heat generating region thereon including the steps of taking a laser probe and roughening the surface of the probe which defines the nominal laser radiation region thereof; applying a coating of infrared absorbing material to the roughened surface whereby said material collects in the uneven recesses defined in the roughened surface region; and applying a protective laser transmissive coating over the infrared absorbing coating.

It is therefore an object of the present invention to provide a medical probe which is capable of performing tissue incision or vaporization at power levels lower than required by conventional laser probe.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is an elevation view, part in section, of the probe of the present invention and a holding member therefor;

Figure 2 is an elevation view showing the probe of Figure 1 inserted into tissue;

Figure 3 is an enlarged sectional view of the probe end showing the heat generating portion thereof;

Figure 4 is a further enlarged sectional view of the probe heat generating portion;

Figure 5 is an elevation view of an alternate embodiment of the probe according to the present invention;

Figure 6 is an elevation view of another alternative embodiment of the probe according to the present invention;

Figure 7 is a perspective view showing an incision of the retina using the probe of Figure 6;

Figure 8 is an elevation view of a yet another alternative embodiment of the probe of the present invention;

Figure 9 is a front elevation view of another embodiment of the probe of the according to the present invention shown installed in the probe connector;

Figure 10 is a side elevational view of the probe shown in Figure 9;

Figure 11 is a front elevation view of the probe of Figure 10 as it appears apart from its mounting connector; and

Figure 12 is an explanatory view of the force-cutting for incision using the probe of Figures 9-11.

PREFERRED EMBODIMENT OF THE INVENTION

Figure 1 is a longitudinal sectional view of a probe 10 according to the present invention which is mounted at the output end of a laser optical fiber 32. The fiber is connected to a source of laser energy (not shown).

Probe 10 is fabricated from a laser transmissible material such as a natural or artificial ceramic material, for example, a natural or artificial sapphire, quartz, or diamond. Polymeric materials may also be employed. In the embodiment as illustrated, the probe 10 comprises a conically tapered main body portion 12 having, at the tip end thereof, a heat generating portion 11 of semi-spherical shape and a mounting portion 14. The main body portion 12 and the mounting portion 14 are formed integrally with each other and a flange 16 is formed between the main body portion 12 and the mounting portion 14. The probe 10 is fitted in a cylindrical female connector 18 and fixed integrally thereto by caulking the mating surfaces thereof or using a ceramic type adhesive between the mating surfaces. The female connector 18 has, on the internal surface thereof, a thread 20 which is adapted to mate with complementary threads 30 of a male connector 22 on the output end of the optical fiber 32. The female connector 18 has two holes 24 through the cylindrical connector wall which facilitate the passage of cooling water W or other fluids there-through. The two holes are circumferentially disposed at angular spaces of 180° although only one of them is shown in Figure 1.

On the other hand, the male connector 22 is press-

edly fitted into a flexible jacket 26 fabricated of, for example, Teflon (trademark). For this press fitting, the male connector 22 has stepped portions 28 at the base portion of the male connector 22 by which the male connector 22 is firmly held by the jacket 26 so as to prevent the former from being disengaged from the latter. As noted, male connector 22 is externally threaded at 30 to mate with the internal thread 20 of the female connector 18.

An optical fiber 32 for transmitting laser energy is inserted into the male connector 22. The optical fiber 32 is disposed concentrically within the jacket 26, leaving a gap 34 therebetween for supplying cooling water. Although the fiber 32 is closely fitted in the male connector 18 at a portion adjacent to the stepped portion of the male connector, the stepped portion 28 has for example two slits 28a formed circumferentially at angular spaces of 180° for letting the cooling water W pass therethrough. A passage 36 for the cooling water W is further provided between the inner face of the tip end portion of the male connector 22 and the optical fiber 32. Cooling water W is fed, according to necessity, through the gap 34 then, in turn, through slit 28a, passage 36 and discharged through the opening 24 to cool the tissue to be treated.

A laser generating unit (not shown) is optically coupled to the input end of fiber 32. A 40 watt laser is common although tissue vaporization can be effected using probes of the present invention with laser powers in the order of 10 watts or less. The laser beam from the laser generating unit is guided through the optical fiber 32 and coupled from the output end thereof to the probe 10 through the base end face 38 thereof. The laser energy is then radiated from the outer face of the probe tip or, as discussed in more detail below, absorbed by the material coating the probe tip.

Figure 2 illustrates the dispersion and diffusion of laser energy when the probe of the present invention is employed. As the main body portion 12 of the probe 10 is formed in a conically tapered shape, some of laser energy may leak from the tapered face but the majority of the laser energy is reflected from the tapered face towards the tip end thereof. Thus, the laser beam is effectively focused and concentrated at the tip region 11 from which point the laser energy is either radiated or absorbed. Region 11 defines the heat generating portion of probe 10.

The outer surface of the heat generating portion 11 of the probe is frosted or roughened as shown in Figures 3 and 4 thereby forming an uneven and irregular contour defining apertures or recesses therein having diameter and depth of 1 to 100 μm , preferably 10 to 60 μm . The frosting or roughening process is preferably carried out by use of a computer controlled grinding wheel. More specifically, the probe undergoing surface treatment is rotated and then brought into contact with a diamond grindstone. The grindstone traces the unroughened contour of the probe, commencing from the tip of the probe, as far rearward along the conical

surface as desired to define the heat generating portion 11 thereof. The computer controls, in a conventional manner, the position and speed of travel of the grindstone. In one preferred arrangement, a grindstone having particles of between 10 to 20 μm is utilized while the grindstone is moved along the probe between 3 and 6 mm/second. This results in a roughened surface contour having approximately 10 μm recesses therein. Of course, other methods may be employed to roughen the probe surface.

In the event that the depth of the recesses defining the roughened surface are too small, the amount of the infrared absorbing material held therein is correspondingly small thereby rendering the heat generating effect insufficient. Conversely, if the surface roughening is too large, excessive heat absorbing material will be retained with a corresponding decrease in the direct laser irradiation of the tissue and an increase in probe tip heating. It is preferable to roughen the tip surface within the limits set out above to maintain a proper balance between direct laser irradiation and indirect heating caused by laser absorption at the probe tip.

Referring to Figure 4, the infrared absorbing material 112 is received and held in the concaved portions 111 formed by the frosting or roughening process. Various compositions may be used for the infrared absorbing material including MnO_2 , Fe_3O_4 , CoO , and Cr_2O_3 . The preferred material is manganese dioxide due to its high melting point. Graphite or carbon may also be utilized although these materials may exhibit oxidation. The particle size of the infrared absorbing material is small, typically 10 μm or less. To attach the infrared absorbing material to the frosted or roughened surface of the main body portion 12 of the probe 10, the tip end portion of the main body portion 12 is dipped in a suspension of the infrared absorbing material. As a dispersion medium, there can be suitably used water or alcohol due to their rapid drying rate. The density of the infrared absorbing material may be selected by controlling the concentration of the dispersion and/or the temperature of the dispersion for obtaining desired heat generation level. When homogeneous dispersion can not be obtained, or a surface active agent is added to the dispersion.

Alternatively, cotton impregnated with the infrared absorbing material, or preferably a dispersion of the infrared absorbing material, may be used to transfer the infrared absorbing material to the frosted or roughened surface of the probe. More specifically, 1/2cc of powder is mixed in approximately 1cc of water. Dry cotton is dipped into the powder suspension so that the cotton can absorb the powder evenly. Excess water is squeezed from the cotton before the impregnated cotton is pressed and rubbed onto the roughened tip surface. A clean piece of cotton is used to softly rub the probe tip region to remove excess powder thereon.

The infrared absorbing material 112 deposited in the concaved portions 111 of the frosted or roughened surface is preferably covered by a coating 113 to pre-

vent damage to the absorbing material during normal use.

Although the material of the coating 113 is not critical so long as it exhibits transmissivity to laser energy as well as suitable heat resistance; an amorphous non-alkali glass or a ceramic such as silica, polyalumina, is preferably utilized. The compound ZrO_2SiO_2 has been found to be quite satisfactory and is mixed with isopropyl alcohol to form a solution (20% ZrO_2SiO_2) therewith. The protective overcoat solution may be applied in substantially the same manner as that described for the absorbing powder. Cotton is dipped into the solution and lightly painted over the powdered tip area. The probe is permitted to dry at room temperature for approximately 30 minutes, then, baked at $150^\circ C$ for another 30 minutes. The above described overcoating steps are repeated until a thickness of between 1 μm and 5 μm is achieved.

Figure 4 illustrates the action of the roughened, impregnated tip on an incident laser beam as the beam attempts to pass through the tip region. As the laser beam enters the heat generating portion 11, the laser energy is irregularly reflected from both the randomly spaced infrared absorbing particles 112 and the surface of the concave portions 111 of the probe tip. The laser energy is partially attenuated by the heat absorbing material with the remainder ultimately being radiated from the tip. This laser energy irradiates and penetrates the adjacent tissue in the conventional manner. That portion of the laser energy absorbed is converted to heat which, in turn, raises the temperature of the heat generating tip portion 11. Although the precise temperature of this tip region depends upon the density of the infrared absorbing material adhering to the surface of the heat generating portion and the laser power, temperatures between about 500 and $700^\circ C$ are typical for probes prepared as set forth herein. It will be appreciated that such elevated probe tip temperatures substantially accelerate the vaporization of the tissue contacted by the probe.

Although the heat generating portion 11 is shown only at the semispherical portion of the tip end of the main body 12 in the foregoing embodiment, it may be provided at other parts of the tapered portion or along its entire length as shown at 11 in Figure 6. In this case, the tapered portion is also frosted or roughened so that the percentage of the laser beam reaching the probe tip is reduced while the percentage of overall probe laser radiation is increased. The modified probe 10A of Figure 6 is suitably used, for example, for selectively effecting incision of retina 52 (Figure 7) without making incision of choroidea 51 due to the vaporization effect of heat generation at the tapered portion when the retina 52 is detached from the choroidea 51 of the eyeground.

The probe may alternatively have a round shape as shown in Figure 8. Probe 10B has a semispherical end provided with the heat absorbing material, as discussed above, at 11. This probe is suitably employed for vaporization and incision of, for example, a constricted part of

an esophagus.

The configuration of the probe may alternatively be such that the opposite sides of the tip end of a cylinder are bevelled thereby defining a wedge-shaped end as shown in Figures 9 to 12. This type of probe 10C may be used in such a manner that it is strongly pressed against the tissue M to make force-cutting for effecting the incision of the tissue M.

The length of the heat generating portion 11 of the probe 10 as illustrated in Figures 1 to 10 may be suitably determined according to the injection depth of the probe into the tissue M and it may in general be within a range of from 1.0 to 7.0 mm. Although the tip end of the heat generating portion 11 is not always required to be in semispherical shape, a pointed end of the heat generating portion would possibly be broken and therefore the tip end of the heat generating portion is preferably be rounded. The flange 16 as described before functions as an abutment or stop for positioning of the probe 10 in the tissue M when the probe 10 is injected into the tissue M until the forward end face of the projected flange 16 abuts against the tissue M. However, the flange 16 may of course be omitted.

Figure 13 illustrates a further form of the probe in which the heat generating portion 11 is extended to the intermediate portion of the taper. This type of probe 10D may be fitted to a surgical contact scalpel.

Claims

1. A medical laser probe (10) for conveying energy from the output end of an optical laser waveguide (32) to a tissue undergoing laser treatment, the probe comprising laser transmissive material having a laser energy input region for receiving laser energy from the optical waveguide and a laser energy radiation surface (11), the laser energy from the input region being propagated through the probe transmissive material to be incident on the probe radiation surface, characterised in that an infrared absorbing coating (112) is applied to and conforming with the laser energy radiation surface for converting a predetermined percentage of the laser energy incident thereon into heat energy, whereby the increased temperature of the probe radiation surface will enhance tissue vaporisation and whereby the laser energy entering the probe not converted to heat energy by the infrared absorbing coating irradiates tissue adjacent the radiation surface.
2. A medical laser probe as claimed in claim 1 characterised in that the infrared absorbing coating (112) is covered by a coating (113) of a laser transmissive material.
3. A medical laser probe as claimed in claim 1 or 2, characterised in that the probe radiating surface (11) has an irregular and uneven contour defining

concave recesses (111) for irregularly refracting and reflecting the laser energy incident thereon and for receiving the infrared absorbing coating in said concave recesses.

4. A medical laser probe as claimed in claim 3, characterised in that the concave recesses (111) defining the uneven surface contours range between 1 and 100 microns. 5
5. A medical laser probe as claimed in any one of claims 1 to 4, characterised in that said infrared absorbing coating (112) is selected from graphite, carbon, clay and titanium oxide, magnesium oxide and iron oxide. 10
6. A medical laser probe as claimed in any one of claims 1 to 5, characterised in that the infrared absorbing coating (112) is a powder material having granule sizes less than about 10 microns. 15
7. A medical laser probe as claimed in any one of claims 2 to 6, characterised in that the laser transmissive coating (113) is made of amorphous non-alkali glass. 20
8. A medical laser probe as claimed in any one of claims 2 to 6, characterised in that the laser transmissive coating (113) is ZrO_2 SiO_2 . 25
9. A process for making a medical laser surgical probe having a heat generating region thereon including the steps of taking a laser probe (10) according to claim 1 and roughening the surface of the probe (11) which defines the nominal laser radiation region thereof; applying a coating of infrared absorbing material (112) to the roughened surface whereby said material collects in the uneven recesses defined in the roughened surface region; and applying a protective laser transmissive coating (113) over the infrared absorbing coating. 30
10. A process as claimed in claim 9, characterised by the steps including the steps of taking the laser probe (10) and grinding the surface (11) of the probe which defines the nominal laser radiation region thereof to create an irregular, uneven contour having concave (111) recesses of between 1 and 100 microns; taking a powder of laser absorbing material (112) comprising particles of less than 10 microns in diameter and preparing a suspension thereof; dipping an applicator into the suspension and stroking the applicator with the infrared absorbing material therein against the uneven probe surface contour thereby depositing absorbing material in the concave recesses defined therein. 35
11. A process as claimed in claim 10 characterised by the further steps of preparing an alcohol solution 40

containing a soluble ceramic amorphous compound; applying the solution over the uneven surface contour containing the laser absorbing material and drying the laser probe to remove the alcohol therefrom. 45

Patentansprüche

1. Medizinische Lasersonde (10) zum Übermitteln von Energie vom Auslaßende eines optischen Laserlichtwellenleiters (32) zu einem mit Laser zu behandelnden Gewebe, wobei die Sonde: laserdurchlässiges Material mit einem Laserenergieeinlaßbereich zum Aufnehmen der Laserenergie vom optischen Wellenleiter und eine Laserenergieabstrahlungsoberfläche (11) aufweist, wobei die Laserenergie vom Einlaßbereich durch die Sonde aus durchlässigem Material geführt wird, um auf die Sondenabstrahlungsoberfläche aufzutreffen, dadurch gekennzeichnet, daß eine infrarotabsorbierende Beschichtung (112) entsprechend der Laserenergieabstrahlungsoberfläche zum Umwandeln eines vorbestimmten Prozentsatzes der darauf auftreffenden Laserenergie in Wärmeenergie eingebracht ist, wobei die erhöhte Temperatur der Sondenstrahlungsoberfläche die Gewebeverdampfung erhöhen wird und wodurch die in die Sonde eingebrachte Laserenergie, die nicht durch die infrarotabsorbierende Schicht in Wärmeenergie umgewandelt wird, Gewebe benachbart zur Abstrahlungsoberfläche bestrahlt. 50
2. Medizinische Lasersonde nach Anspruch 1, dadurch gekennzeichnet, daß die infrarotabsorbierende Beschichtung (112) mit einer Schicht (113) eines laserdurchlässigen Materials bedeckt ist. 55
3. Medizinische Lasersonde nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß die Abstrahlungsoberfläche der Sonde (11) einen unregelmäßigen und unebenen Umriß besitzt, der konkave Vertiefungen (111) zur irregulären Refraktion und Reflexion der auftreffenden Laserenergie und zum Aufnehmen der infrarotabsorbierenden Beschichtung in diesen konkaven Vertiefungen bestimmt.
4. Medizinische Lasersonde nach Anspruch 3, dadurch gekennzeichnet, daß die konkaven Vertiefungen (111), die den unebenen Oberflächenumriß bestimmen, zwischen 1 und 100 µm liegen.
5. Medizinische Lasersonde nach einem der Ansprüche 1 bis 4, dadurch gekennzeichnet, daß die infrarotabsorbierende Beschichtung (112) aus Graphit, Kohlenstoff, Tonerde und Titanoxid, Magnesiumoxid und Eisenoxid ausgewählt ist.
6. Medizinische Lasersonde nach einem der Ansprüche 1 bis 5, dadurch gekennzeichnet, daß die infra-

rotabsorbierende Beschichtung (112) ein Pulvermaterial mit Korngrößen unter 10 µ ist.

7. Medizinische Lasersonde nach einem der Ansprüche 2 bis 6, dadurch gekennzeichnet, daß die laserdurchlässige Beschichtung (113) aus einem amorphen alkalifreien Glas hergestellt ist.
8. Medizinische Lasersonde nach einem der Ansprüche 2 bis 6, dadurch gekennzeichnet, daß die laserdurchlässige Beschichtung (113) ZrO_2SiO_2 ist.
9. Verfahren zum Herstellen einer chirurgischen medizinischen Lasersonde, die einen wärmeentwickelnden Bereich darauf besitzt, das die Schritte beinhaltet:

Vorlegen einer Lasersonde (10) nach Anspruch 1 und Aufrauen der Oberfläche der Sonde (11), wodurch der nominale Laserabstrahlungsbereich derselben definiert wird;
Aufbringen einer Schicht eines infrarotabsorbierenden Materials (112) auf die aufgerauhte Oberfläche, wobei das Material sich in den unebenen Vertiefungen, die im aufgerauhten Oberflächenbereich enthalten sind, sammeln; und
Aufbringen einer schützenden laserdurchlässigen Schicht (113) über der infrarotabsorbierenden Schicht.

10. Verfahren nach Anspruch 9, gekennzeichnet durch die Schritte, die die Schritte:

Vorlegen der Lasersonde (10) und Schleifen der Sondenoberfläche (11) der Sonde, die den nominalen Laserabstrahlungsbereich desselben definiert, um einen irregulären, unebenen Umriß mit konkaven Vertiefungen (111) von zwischen 1 und 100 µm zu bilden;
Vorlegen eines Pulvers aus laserabsorbierendem Material (112), das Partikel eines Durchmessers von weniger als 10 µ aufweist und Herstellen einer Suspension davon;
Eintauchen eines Applikators in die Suspension; und
Bestreichen des unebenen Sondenoberflächenumrisses mit dem Applikator mit dem infrarotabsorbierenden Material, um dabei absorbierendes Material in den darin definierten konkaven Vertiefungen abzulagern.

11. Verfahren nach Anspruch 10, gekennzeichnet durch die weiteren Schritte:

Herstellen einer alkoholischen Lösung, die eine lösliche amorphe keramische Verbindung enthält;
Auftragen der Lösung auf den unebenen Ober-

flächenumriß, (die das laserabsorbierende Material enthält) und Trocknen der Lasersonde zum Entfernen des Alkohols.

Revendications

1. Sonde laser à usage médical (10) pour transporter de l'énergie à partir d'une extrémité émettrice d'un guide d'onde laser optique (32) vers un tissu soumis à un traitement laser, sonde comprenant un matériau conducteur de rayonnement laser comportant une région réceptrice d'énergie laser pour recevoir de l'énergie laser à partir du guide d'onde optique et une surface rayonnante d'énergie laser (11), l'énergie laser provenant de la région émettrice étant propagée à travers le matériau conducteur de la sonde suivant un parcours incident à la surface rayonnante de la sonde, sonde caractérisée en ce qu'un revêtement absorbant dans l'infrarouge (112) est appliqué de manière à épouser la surface rayonnante d'énergie laser en vue de convertir un pourcentage prédéterminé d'énergie laser incidente à la surface en énergie thermique, de sorte que l'élévation de température de la surface rayonnante de la sonde favorise la vaporisation du tissu et de sorte que l'énergie laser pénétrant dans la sonde non convertie en énergie thermique par le revêtement absorbant dans l'infrarouge irradie le tissu adjacent à la surface rayonnante.
2. Sonde laser à usage médical selon la revendication 1, caractérisée en ce que le revêtement absorbant dans l'infrarouge (112) est recouvert d'un revêtement (113) de matériau conducteur de rayonnement laser.
3. Sonde laser à usage médical selon la revendication 1 ou 2, caractérisée en ce que la surface rayonnante de la sonde (11) présente un contour irrégulier et non uniforme décrivant des replis concaves (111) destiné à réfracter et à réfléchir l'énergie laser incidente à la surface et à recevoir le revêtement absorbant dans l'infrarouge dans lesdits replis concaves.
4. Sonde laser à usage médical selon la revendication 3, caractérisée en ce que les replis concaves (111) que décrit la surface non uniforme mesurent de 1 à 100 µm.
5. Sonde laser à usage médical selon l'une quelconque des revendications 1 à 4, caractérisée en ce que ledit revêtement absorbant dans l'infrarouge (112) est choisi parmi le graphite, le carbone, l'argile et l'oxyde de titane, l'oxyde de magnésium et l'oxyde de fer.
6. Sonde laser à usage médical selon l'une quelconque des revendications 1 à 5, caractérisée en ce

que le revêtement absorbant dans l'infrarouge (112) est un matériau pulvérulent de granulométrie inférieure à 10 µm environ.

7. Sonde laser à usage médical selon l'une quelconque des revendications 2 à 5, caractérisée en ce que le revêtement conducteur de rayonnement laser (113) est fabriqué en verre amorphe non alcalin. 5
8. Sonde laser à usage médical selon l'une quelconque des revendications 2 à 6, caractérisée en ce que le revêtement conducteur de rayonnement laser (113) est en $ZrO_2 - SiO_2$. 10
9. Procédé de fabrication d'une sonde laser chirurgicale à usage médical dotée en surface d'une région génératrice de chaleur comprenant les étapes consistant à obtenir une sonde laser (10) selon la revendication 1 et à dépolir la surface de la sonde (11) qui définit la région rayonnante d'énergie laser nominale; à appliquer un revêtement de matériau absorbant dans l'infrarouge (112) à la surface dépolie de manière à ce que ledit matériau s'accumule dans les replis non uniformes que décrit la région de surface dépolie, et à appliquer un revêtement protecteur conducteur de rayonnement laser (113) sur le revêtement absorbant dans l'infrarouge. 15 20 25
10. Procédé selon la revendication 9, caractérisé en ce qu'il comporte les étapes consistant à obtenir la sonde laser (10) et à dépolir la surface (11) de la sonde qui définit la région rayonnante d'énergie laser nominale en vue de former un contour irrégulier non uniforme présentant des replis concaves (111) mesurant de 1 à 100 µm; à obtenir une poudre de matériau absorbant de rayonnement laser (112) comprenant des particules de diamètre inférieur à 10 µm pour en préparer une suspension; à tremper un applicateur dans la suspension et à frotter l'applicateur contenant le matériau absorbant dans l'infrarouge contre la surface de la sonde de contour non uniforme de manière à déposer le matériau absorbant dans les replis concaves que décrit la surface. 30 35 40 45
11. Procédé selon la revendication 10, caractérisé en ce qu'il comporte en outre les étapes de préparation d'une solution alcoolique contenant un composé céramique amorphe soluble; d'application de la solution contenant le matériau absorbant de rayonnement laser sur la surface de contour non uniforme et de séchage de la sonde laser afin d'en éliminer l'alcool. 50 55

FIG. 1

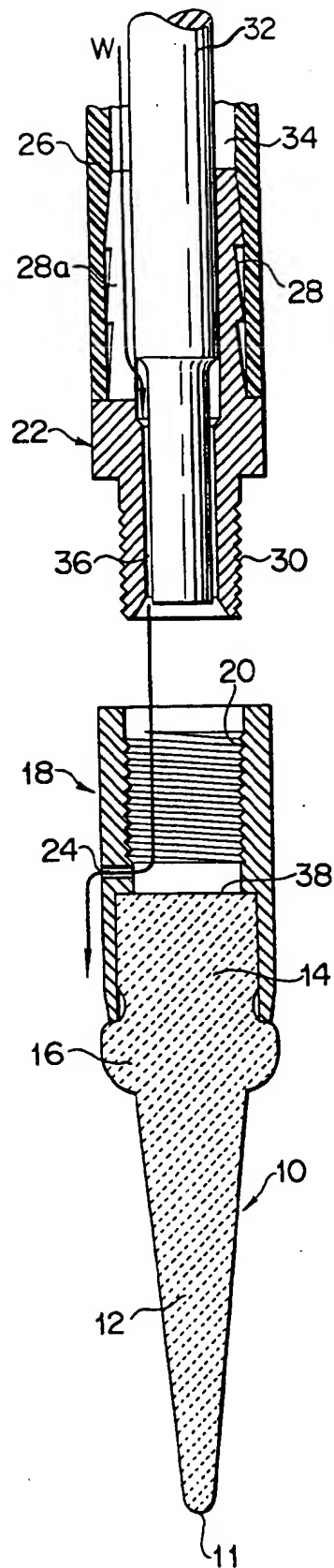


FIG. 2

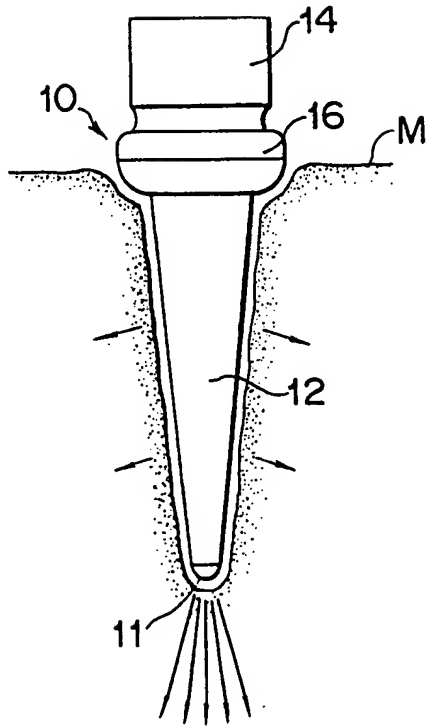


FIG. 3

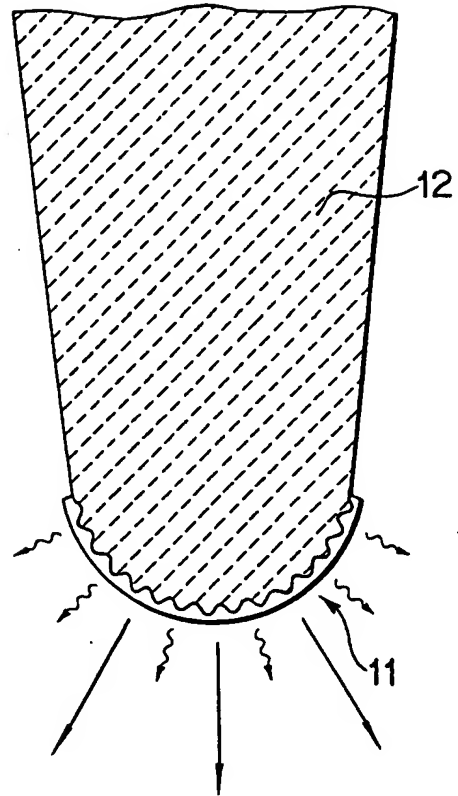


FIG. 4

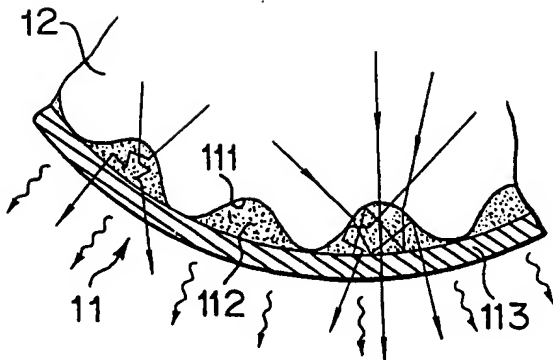


FIG. 6

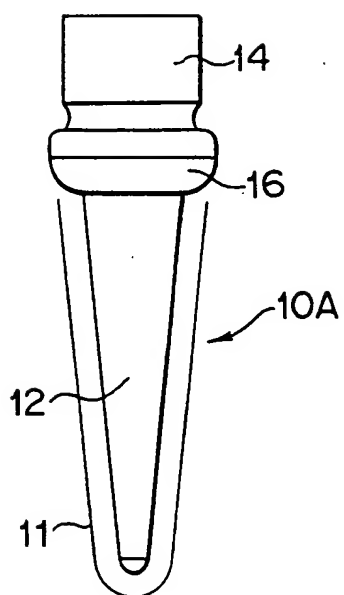


FIG. 7

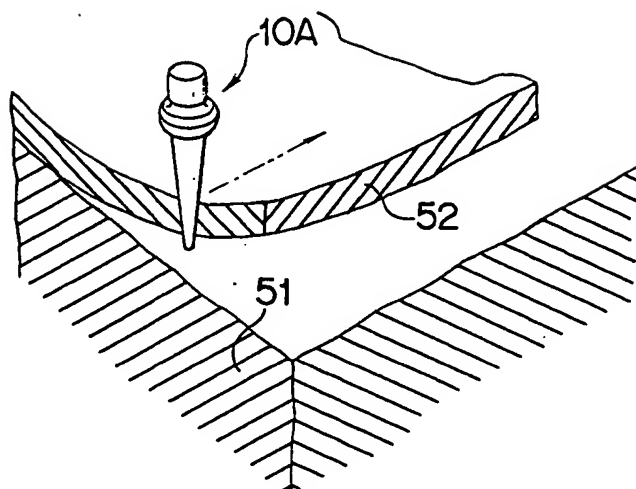


FIG. 9

FIG. 8

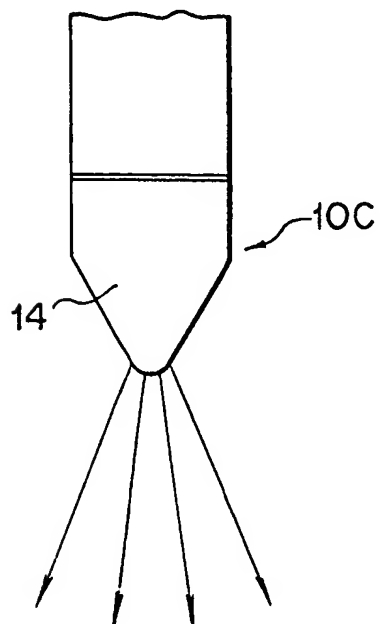
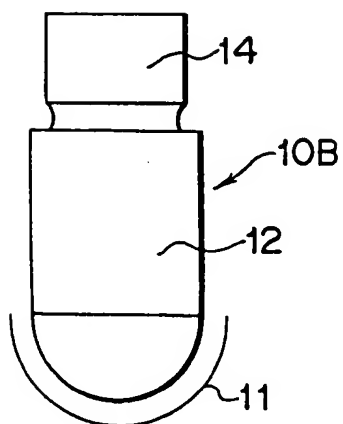


FIG. 10

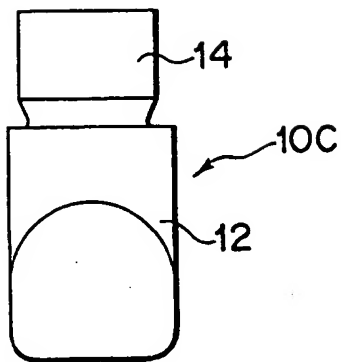


FIG. 11

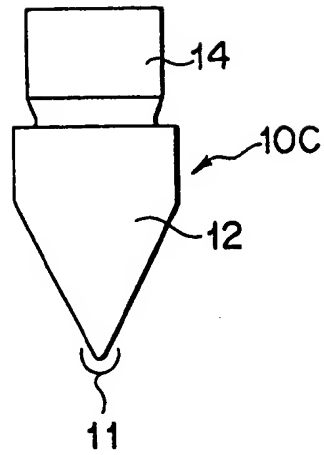


FIG. 5

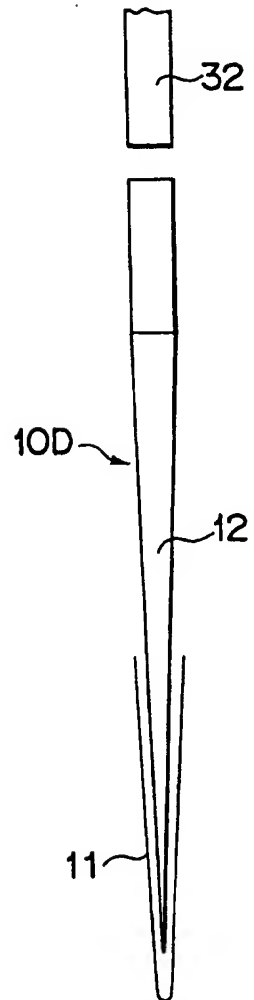


FIG. 12

